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## MATERIALS SCIENCE & ENGINEERING

# Possible explanation for trapped field enhancement on REBaCuO bulk by modified multi-pulse technique with stepwise cooling (MMPSC)

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#### ABSTRACT

The time evolutions of the local fields  $B_L(t)$  have been measured on the surface of the superconducting bulk disk magnetized by a two-stage pulse-field magnetizing technique, called a modified multi-pulse technique combined with stepwise cooling (MMPSC), and the magnetic flux movement and the flux trapping have been investigated. The optimum concaved ("*M*-shaped") trapped field profile, which is a necessary condition at the first stage to enhance the final trapped field  $B_T$ , makes a larger magnetic gradient (d*B*/dx) at the bulk periphery in the ascending stage of the applied magnetic pulse at the second stage due to the large viscous force  $F_v$ . The magnetic fluxes, which stay at the bulk periphery, start to flow to the center of the bulk, after the applied pulse field reaches a maximum, at which the flux velocity *v* is nearly zero and then  $F_v$  decrease. As a result, a large number of the magnetic fluxes are trapped at the bulk center. The effect of the "M-shaped" profile at the first stage in MMPSC on the enhancement of  $B_T$  is discussed.

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#### 1. Introduction

Recently, a pulse field magnetization (PFM) for REBaCuO bulks (RE: rare earth element and Y) has been intensively investigated for practical applications, instead of a field-cooled magnetization (FCM), because PFM is an inexpensive and mobile experimental setup with no use of a superconducting magnet. The trapped field  $B_{\rm T}^{\rm P}$  by PFM is, however, lower than that by FCM at temperatures lower than 50K due to the large temperature rise by the dynamical motion of the magnetic fluxes. At 77 K, several approaches have been performed and succeeded to enhance  $B^{\rm P}_{\rm T}$  by an iteratively magnetizing pulsed-field method with reducing amplitude (IMRA)[1], a multi-pulse technique with stepwise cooling (MPSC) [2] and so on. We have systematically studied the time and spatial dependences of the temperature T(t,x), local field  $B_{\rm I}(t)$  and the trapped field  $B_{\rm T}^{\rm P}$ on the surface of cryocooled REBaCuO bulks 45 mm in diameter during PFM for various starting temperatures  $T_s$  and applied fields  $B_{\text{ex}}$  [3–5]. To enhance  $B_{\text{T}}^{\text{P}}$ , the reduction in temperature rise  $\Delta T$  is an indispensable issue. The lowering of  $T_s$  is also effective because the critical current density  $I_c$  and resultant trapped field  $B_T^P$  increase with lowering  $T_s$ . However, in the PFM technique, the lowering of  $T_{\rm s}$  as low as 10–20 K is not necessarily effective because of the large heat generation due to the enhancement of pinning loss and the decrease in the heat capacity of the bulk [6]. Taking the obtained experimental results into consideration, we proposed a new PFM technique named as a modified MPSC (MMPSC), which consisted of the two-stage procedures [7]. In this technique, a small number of magnetic fluxes should be trapped on the bulk periphery for the reduction in  $\Delta T$  at a first stage at T1 (<T<sub>c</sub>), and the optimum pulse field B2 should be applied at a second stage at T2 (<T1). The "M-shaped" trapped field profile, which means the lower trapped field at the bulk center than that at the bulk periphery, is also necessary at the first stage to enhance  $B_T^P$ . Using the MMPSC method, we have succeeded a highest field trapping of  $B_T^P = 5.20$  T on the  $\phi$ 45 mm GdBaCuO bulk, on which 3.6 T had been trapped by a single pulse application at 40 K [8].  $B_T^P$  = 5.20 T is a record-high value by PFM to date. The MMPSC method has been proved to be a universal and effective method to enhance  $B_{T}^{P}$  using other bulks such as the  $\phi$ 45 mm SmBaCuO disk with different pinning ability [9], the rectangular-shaped GdBaCuO bulk  $(33 \text{ mm} \times 33 \text{ mm} \times 15 \text{ mm})$  [10] and the large GdBaCuO disk 65 mm in diameter [11]. In the previous study, we measured the time evolutions of the local fields  $B_{I}(t)$ at three points on the bulk surface [8] and the two-dimensional trapped field profile just above 0.5 mm on the bulk for various  $B_{ex}$ and  $T_{\rm s}$  [12]. It has been found that the "M-shaped" profile should be experimentally optimized to enhance  $B_{T}^{P}$ . However, there has been no reasonable explanation for the question, why the "M-shaped" profile is necessary at the first stage in MMPSC.

In this paper, we measure the time evolutions of the local fields  $B_L(t)$  at several points on the bulk surface for various conditions in

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Fig. 1. (a) The experimental setup around the bulk and the pulse coil. Three Hall sensors are adhered at #1, #2 and #3 on the surface of the bulk. (b) The experimental sequence of the MMPSC method, where the estimated time dependence of the temperature is shown.

the MMPSC process, and analyze the magnetic flux movement and trapping. The meaning of the "M-shaped" profile at the first stage in MMPSC is discussed.

#### 2. Experimental

The GdBaCuO bulk disk (Nippon Steel, Japan) used in this study was 45 mm in diameter and 18 mm in thickness, which was different from that attained  $B_T = 5.20 \text{ T}[8]$ . Fig. 1(a) shows the experimental setup around the bulk and the magnetizing pulse coil. The bulk was mounted on soft iron yoke cylinder 40 mm in diameter and 20 mm in thickness and tightly anchored onto the cold stage of a Gifford-McMahon (GM) cycle helium refrigerator. The temperature of the bulk was controlled over the range from 30K to 70 K. The magnetizing solenoid coil, which generated the pulse field up to  $B_{ex} = 6.3$  T with a rise time of 12 ms, was placed outside the vacuum chamber, in which the central axis of the resulting field coincides with that of the bulk. The trapped field characteristics of the bulk by the single pulse application have been reported elsewhere [12]. Fig. 1(b) shows the experimental sequence of the MMPSC technique. Four magnetic pulses were applied at different initial temperatures T1 and T2 on the bulk surface. At the first stage, a pulse field B1 was applied twice at T1 (=70 K or 30 K) in order to realize various shapes of the trapped field profile on the bulk. Hereafter, we refer to these two pulses as Nos. 1 and 2. At the second stage, the bulk was cooled down to T2 (=30K) and a higher pulse field B2 (=6.3 T) was applied twice (Nos. 3 and 4), after recovering to T2. Three Hall sensors (F.W. Bell, model BHT 921) were adhered in a line at the positions #2 (bulk center), #1 and #3 (12.5 mm distant from the bulk center) on the bulk surface as shown in Fig. 1(a). For each pulse of the MMPSC method, the time evolutions of the local fields  $[B_{I}(\#1)(t), B_{I}(\#2)(t)]$  and  $B_{I}(\#3)(t)$  were monitored by using a digital oscilloscope. The trapped field profile  $B_{\rm T}(2\,{\rm mm})$  was measured 2.0 mm above the bulk surface by scanning an axial-type Hall sensor (F.W. Bell, BHA 921) inside the vacuum chamber using

a scanning device, which has an x-y stage controller with a flexible bellows. The trapped field profiles  $B_T(0.5 \text{ mm})$  were also measured 0.5 mm above the bulk surface under the same MMPSC conditions, after removing the adhered Hall sensors.

#### 3. Results and discussion

#### 3.1. Trapped field profiles at the first stage for various conditions

In the MMPSC method, a desired trapped field profile at the first stage can be controlled by choosing the conditions of *T*1 and *B*1, and the subsequent trapped field profile of the second stage is realized by *T*2 and *B*2. Table 1 summarizes four cases (Case A–Case D) and their conditions (*T*1, *B*1, *T*2 and *B*2) investigated in this study. Four trapped field profiles with different shape were realized at the first stage and, at the second stage, the magnetic flux movement and the trapping were measured after the pulse field application of *B*2 = 6.3 T at *T*2 = 30 K. In the Case D, the pulse fields were not applied at the first stage and the pulse field of *B*2 = 5.7 T was applied twice to the virgin state bulk at *T*2 = 30 K.

Fig. 2(a) shows the vertical sections of the  $B_T(0.5 \text{ mm})$  profile along different directions and the trapped fields [ $B_T(\#1)$ ,  $B_T(\#2)$ and  $B_T(\#3)$ ] after applying pulse field of B1 = 3.2 T at T1 = 70 K (No. 1 pulse of the Case A). The two-dimensional  $B_T(0.5 \text{ mm})$  profile is also shown in the inset. The vertical sections are nearly symmetric, which suggest that the trapped field profile can be estimated using three Hall sensors at #1, #2 and #3. Fig. 2(b) shows the trapped field profiles from Case A to Case D at the end of the first stage. The measured  $B_T$  values at the positions from #1 to #3 and the estimated ones ( $B_T = 0$ ) at the bulk edge (X = 22.5 mm) were used. In the Cases B and C, a "large M" and a "trapezoid"  $B_T$  profiles were realized, respectively. In the Case A, the M-shaped profile was somewhat smaller than that in the Case B, in which the maximum  $B_T(\#2)$  as high as 4.0T was finally obtained. We abbreviate the  $B_T$  profile in the Case A as "optimum M".

#### Table 1

The conditions (T1, B1, T2 and B2) and the final trapped field  $B_{T}$  (#2) from Case A to Case D in the MMPSC method

	1st stage ( <i>T</i> 1 and <i>B</i> 1) (No. 1 and No. 2)	2nd stage ( <i>T</i> 2 and <i>B</i> 2) (No. 3 and No. 4)	<i>B</i> <sub>T</sub> (#2) (No. 4)
Case A (optimum M)	70 K, 3.2 T (No. 1)	30 K, 6.3 T	4.0 T
	70 K, 3.2 T (No. 2)		
Case B (large M)	30 K, 6.2 T (No. 1)	30 K, 6.3 T	1.5 T
	30 K, 6.2 T (No. 2)		
Case C (trapezoid)	70 K, 3.9 T (No. 1)	30 K, 6.3 T	1.2 T
	30 K, 4.6 T (No. 2)		
Case D (without)	-	30 K, 5.7 T	1.2 T



**Fig. 2.** (a) The example of vertical sections of the  $B_T(0.5 \text{ mm})$  profile along different directions and  $B_T$  at #1, #2 and #3 after applying pulse field of B1 = 3.2 T at T1 = 70 K. (b) The trapped field profile at the first stage in MMPSC method for the cases from Case A to Case D.

#### 3.2. The flux movement and flux trapping at the second stage

The flux movement and the flux trap are investigated on the bulk with different trapped flux distribution from Case A to Case D, after applying the No. 3 pulse of B2 = 6.3 T (=5.7 T in the Case D)at T2 = 30 K. Fig. 3 shows the results for the Case A. In Fig. 3(a), the time evolutions of the applied field  $\mu_0 H_a(t)$  and the local fields  $B_1(t)$ at #1, #2 and #3 are shown. The applied field smoothly increased and took a maximum at t = 12 ms and then decreased.  $B_{I}(\#1)(t)$  and  $B_{\rm I}(\#3)(t)$  started to rise at  $t=6\,{\rm ms}$  with a time delay and took a maximum at t = 15 and 17 ms, respectively.  $B_{I}(\#2)(t)$  started to rise at t = 13 ms with a long time delay, took a maximum at t = 17 ms and then decreased. The magnitude of  $B_L(\#2)(t)$  is larger than that at #1 and #3 for t > 20 ms. Fig. 3(b) and (c) shows the time dependences of the transient magnetic distribution for the ascending ( $t \le 12 \text{ ms}$ ) and the descending  $(t \ge 12 \text{ ms})$  stages of the No. 3 pulse field, respectively, both of which were reconstructed using  $B_{I}(t)$  at #1, #2 and #3 shown in Fig. 3(a).  $B_{I}(\#1)(t)$  and  $B_{I}(\#3)(t)$  hardly change for  $t \le 6$  ms and the magnetic flux distribution in the bulk showed a kink at #1 and #3. This result cannot be explained using a Bean's critical-state model under zero-field cooling, because the magnetic gradient  $dB_L/dx$ , which is proportional to a critical current density J<sub>c</sub>, should be constant along the radius direction and the flux distribution should be expressed by a straight line. This result strongly suggests that the viscous force  $F_{\nu}$  for the flux movement is strong early in the ascending stage. For  $t \ge 6$  ms,  $B_{\rm L}(\#1)(t)$  and  $B_{\rm L}(\#3)(t)$ gradually increase and the flux distribution changes to a straight line. The  $B_{\rm L}(\#2)(t)$  value slightly increases during the ascending stage. For the descending stage as shown in Fig. 3(c), however,  $B_L(#2)(t)$  sharply increased at t = 15 ms, just after the applied field  $\mu_0 H_a(t)$  took a maximum.  $B_L(t)$  at #1 and #3 gradually decreased with increasing time and a cone-shaped trapped field distribution with  $B_T^P = 4.0$  T was finally obtained.

Fig. 4 shows the similar results for the Case B, where a large M-shaped trapped-field profile was realized at the first stage. In Fig. 4(a),  $B_L(\#1)(t)$  and  $B_L(\#3)(t)$  started to rise at t = 6 ms and then took a maximum of 4.5 T at t = 13 ms. The maximum value was smaller, and the time, at which  $B_L(t)$  took a maximum, was shorter than that for the Case A. In Fig. 4(b) and (c),  $B_L(\#1)(t)$  and  $B_L(\#3)(t)$  smoothly increased and then decreased. As a result, the large M-shaped profile was almost maintained. It should be noted that the magnetic gradient ( $dB_L/dx$ ) at the end of the ascending stage (t = 12 ms) was smaller than that for the Case A.

Fig. 5 shows the similar results for the Case C, where a trapezoidshaped trapped field profile was realized at the first stage. In Fig. 5(a),  $B_L(\#1)(t)$  and  $B_L(\#3)(t)$  keep the initial values up to t = 10 ms and then the magnetic fluxes abruptly intrude into the bulk like a flux jump.  $B_L(\#2)(t)$  was not enhanced even at the descending stage, contrary to the Case A. In Fig. 5(b),  $F_v$  is strong for  $t \le 10$  ms and magnetic fluxes cannot intrude into the bulk center. In the descending stage,  $B_L(\#1)(t)$  and  $B_L(\#3)(t)$  decreased with increasing time and the  $B_L(\#2)(t)$  kept a initial value. Since the large temperature rise might take place at the bulk periphery due to the flux jump, the flux flow did not take place to the bulk center but took place to the bulk periphery. As a result, the  $B_T(\#2)$  value was not enhanced only with a slight deformation of the trapped field profile.



**Fig. 3.** (a) The time dependence of the applied field  $\mu_0 H_a(t)$  and the local fields  $B_L(t)$  at #1, #2 and #3 for the No. 3 pulse in the Case A (optimum M). The time dependence of the flux movement in the bulk for (b) the ascending ( $t \le 12 \text{ ms}$ ) and (c) the descending ( $t \ge 12 \text{ ms}$ ) stages of the No. 3 pulse.



**Fig. 4.** (a) The time dependence of  $\mu_0 H_a(t)$  and  $B_L(t)$  at #1, #2 and #3 for the No. 3 pulse in the Case B (large M). The time dependence of the flux movement in the bulk for (b) the ascending ( $t \le 12 \text{ ms}$ ) and (c) the descending ( $t \ge 12 \text{ ms}$ ) stages of the No. 3 pulse.



**Fig. 5.** (a) The time dependence of the  $\mu_0 H_a(t)$  and  $B_L(t)$  at #1, #2 and #3 for the No. 3 pulse in the Case C (trapezoid). The time dependence of the flux movement in the bulk for (b) the ascending ( $t \le 12 \text{ ms}$ ) and (c) the descending ( $t \ge 12 \text{ ms}$ ) stages of the No. 3 pulse.

The similar results for the Case D are indicated in Fig. 6, where a first magnetic pulse was applied to the virgin state bulk as a No. 3 pulse. In the previous paper, the temperature rise for the first pulse-field application is larger, compared with that in the case, where a small number of the magnetic fluxes are already trapped [5]. Then the maximum of  $B_L(\#1)(t)$  and  $B_L(\#3)(t)$  reaches 5 T and  $B_L(\#2)(t)$  increases to 1.5 T due to the large temperature rise. In Fig. 6(b) and (c), the magnetic flux distribution is not a straight line along the radius direction at the end of the ascending stage, and

finally shows the asymmetric M-shaped trapped field profile. The  $B_T^P$  value at the bulk center cannot be enhanced. These results from Figs. 3–6 suggest that the magnetic fluxes enter to the bulk center at the specified trapped field profile at the first stage.

#### 3.3. Possible explanation of $B_T$ enhancement in MMPSC

In the previous subsection, it was clarified that the optimum "M-shaped" profile such as "Case A" should be realized at the first



**Fig. 6.** (a) The time dependence of  $\mu_0 H_a(t)$  and  $B_L(t)$  at #1, #2 and #3 in the virgin state bulk in the Case D (without). The time dependence of the transient magnetic distribution in the bulk for (b) the ascending and (c) the descending ( $t \ge 12 \text{ ms}$ ) stages of the No. 3 pulse.



Fig. 7. The conceptual time dependence of the transient magnetic field distribution for the optimum M-shaped profile (Case A) ((a) and (b)), and for the large M-shaped profile (Case B) ((c) and (d)) for the ascending and the descending stages of the No. 3 pulse field.

stage in MMPSC to enhance  $B_T^P$ . We qualitatively discuss about the magnetic flux movement and trapping after the No. 3 pulse application, compared with the estimated results by a Bean's critical-state model.

The flux motion in the bulk is determined by the force balance in the critical-state model:

$$F_{\rm L} = -(F_{\rm P} + F_{\nu}) = J_{\rm c}B + \eta \frac{B}{\phi_0}V,$$
(1)

where  $F_L$  is the Lorentz force,  $F_P$  the pinning force,  $J_c$  the critical current density, *B* the applied pulse field,  $\eta$  the viscosity coefficient,  $\phi_0$  a fluxoid quantum and v is the flux velocity.  $F_v$  is proportional to v, but  $F_P$  is independent of v.

Fig. 7(a) and (b) shows the conceptual time dependence of the transient magnetic field distribution for the optimum M-shaped profile (Case A) for the ascending and the descending stages of the No. 3 pulse field, respectively, both of which were estimated by use of the results in Fig. 3(b) and (c). In these figures, thin and thick

lines show the distribution for the ZFC method (Bean's criticalstate model) and for the No. 3 pulse application in the MMPSC method, respectively. In the MMPSC method, a large magnetic gradient (dB/dx) exists in the bulk periphery at the ascending stage, which is fairly larger than that estimated by a Bean's critical-state model due to the large viscous force  $F_v$ . When the applied pulse field reaches a maximum at t = 12 ms, a large number of magnetic fluxes, which stay at the bulk periphery, start to flow to the center of the bulk and then the trapped field profile changes from the "*Mshaped*" profile to the "*cone-shaped*" one at the descending stage. At this moment, the flux velocity v is nearly zero and  $F_v$  decreases to zero as estimated from Eq. (1). The magnetic gradient  $\partial B(x,t)/\partial x$  in the bulk can be derived as follows [13]:

$$\frac{\partial B(x,t)}{\partial x} = \mu_0 \pm J_c \frac{B(x,t)}{|B|} + \frac{\eta}{\phi_0 |B| x_{x_0}}^x \frac{\partial B(x',t)}{\partial t} x' \,\mathrm{d}x'. \tag{2}$$

In the ZFC method, since the time dependence of the magnetic field  $\partial B(x',t)/\partial t$  in the bulk is almost zero,  $\partial B(x,t)/\partial x$  is given by  $\mu_0 J_c$ . How-

ever, in PFM, the magnitude of  $\partial B(x,t)/\partial x$  is markedly affected by the presence of the second term in Eq.(2). For instance,  $\partial B(x',t)/\partial t$  is positive in the ascending stage and the second term of Eq.(2) becomes positive. Hence,  $\partial B(x,t)/\partial x$  is enhanced by an amount relative to  $\mu_0 J_c$  in the ZFC method.

Fig. 7(c) and (d) shows the similar conceptual view for the large M-shaped profile (Case B) for the ascending and the descending stages of the No. 3 pulse field. In this case, a large magnetic gradient (dB/dx) exists at the bulk periphery at the end of the ascending stage (t = 12 ms), but the dB/dx value is smaller than that for the optimum M-shaped profile (Case A) due to the higher height at the bulk center of the large M-shaped profile. Then the magnetic fluxes, which stay at the bulk periphery, do not flow to the bulk center, but flow to out of the bulk at the descending stage, even though the flux velocity v is nearly zero and the viscous force  $F_v$  decreases.

Finally, we comment on the influence of the temperature rise on the final trapped field during PFM. In the previous study, it was clarified that the already trapped fluxes in the bulk should reduce the temperature rise due to the decrease of the pinning loss  $Q_{\rm p}$ [5]. In this study, the temperature rise seems to be the largest for Case D ("without") and is the smallest for Case B ("large M"), after applying the No. 3 pulse. The temperature rise for the Case C ("trapezoid") is estimated to be also large because of the flux jump. In this sense, a larger number of the magnetic fluxes should be trapped and the  $B_{\rm T}(\#2)$  value should be enhanced in the Case B. However, the  $B_T^P$  value was not enhanced for the Case B and the optimum "Mshaped" profile such as Case A ("optimum M") exists in MMPSC. These results strongly suggest that a moderate temperature rise is necessary to enhance the  $B_T^P$  value in the MMPSC method. The penetration of the field into the bulk during PFM could have been caused by a combination of heating due to the magnitude of the induced screening currents which corresponds to the slope of the  $B_{\rm L}$  vs. x curve, and a suppression of  $J_c$  by the local field. It is necessary to study the flux dynamics using a theoretical treatment.

#### 4. Summary

The time evolutions of the local fields  $B_L(t)$  have been measured on the surface of the superconducting bulk disk magnetized by a modified multi-pulse technique combined with stepwise cooling (MMPSC) under various trapped field profiles at the first stage, and the magnetic flux movement and the flux trapping have been investigated. The important experimental results and conclusions obtained in this study are summarized as follows:

(1) The trapped field  $B_T^P$  by the MMPSC method strongly depends on the trapped field profile at the first stage. The "M-shaped" profile, which means the higher trapped field at the bulk periphery than that at the bulk center, is a necessary condition to enhance  $B_{T}^{P}$  and should be optimized.

- (2) The time dependences of the flux distribution were reconstructed for the ascending and the descending stages of the applied pulse field using  $B_L(t)$ . These graphs enable us to understand the flux motion and trapping in the bulk clearly.
- (3) Under the optimum M-shaped profile at the first stage, the large viscous force  $F_v$  is created at the end of ascending stage of the No. 3 pulse, at which the temperature rise is relatively small. When the applied pulse field reaches a maximum, at which the viscous force  $F_v$  decreases due to v=0, a large number of magnetic fluxes, staying at the bulk periphery, start to flow to the center of the bulk and then the trapped field profile changes from the "*M-shaped*" to the "cone-shaped" one at the descending stage.
- (4) A moderate amount of temperature rise is necessary to enhance the  $B_T^P$  value at the second stage, which is decided the relations between the trapped field profile at the first stage, *T*2 and *B*2.

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