

## 1. INTRODUCTION

The intermetallic compound of magnesium diboride ( $\text{MgB}_2$ ) has the highest superconducting transition temperature  $T_c=39$  K, which are expected to be applicable in magnetically levitated trains (MAGLEVs) and wind power generators using liquid  $\text{H}_2$  or a cryocooler system.  $\text{MgB}_2$  superconducting bulk also has a promising potential as a quasi-permanent magnet with high-performance, light-weight and homogeneous trapped field distribution superconducting materials.  $\text{MgB}_2$  has a long coherence length compared to RE-Ba-Cu-O (RE: rare earth elements). Therefore, the problem of weak-links at grain boundaries can be ignored and a superconducting bulk magnet using a polycrystal can be realized.

To fabricate a high-performance  $\text{MgB}_2$  superconducting bulk, one important issue is to attain competitive values for critical current density,  $J_c$  under high applied magnetic fields. It has been reported that by enhancement of the filling rate and the decrease of the grains size, the pinning centres at the grain boundaries increase; hence we are able to improve  $J_c$  of the bulk. We have suggested that to improve the filling rate, we can control the grains size in the bulk. The smaller the grains size, the greater the number of the grain boundaries in the bulk. Mortar mixing and ball milling methods were considered which could decrease the grains size. Moreover, the Spark Plasma Sintering (SPS) method strongly influences the filling rate and grain boundaries and also produces nanograined high density bulk materials. In this study, to optimize the mixing and milling conditions, we have investigated the trapped field and superconducting properties of  $\text{MgB}_2$  bulks fabricated by SPS method using  $\text{MgB}_2$  *ex-situ* powder.

## 2. EXPERIMENTAL

$\text{MgB}_2$  *ex-situ* powders (99% in purity) were weighted and mixed using mortar mixing and ball milling machine. The conditions for mortar mixing samples are 1 h, 2 h, 10 h in air atmosphere, and for ball milling conditions are 1 h, 12 h, 48 h at 250 rpm in argon atmosphere. Then the powders were loaded into a graphite die (mortar mixed samples:  $\phi=10$  mm, ball milled samples:  $\phi=20$  mm) and sintered between  $600^\circ\text{C} \sim 1050^\circ\text{C}$  for 5-10 min in vacuum under a mechanical uniaxial pressure and a pulse electrical current of SPS. The applied pressures were 3.93 kN for  $\phi=10$  mm samples and 15.71 kN for  $\phi=20$  mm samples. For sample measurement, the structural characterization was performed using XRD (X-Ray Diffraction). XRD patterns were measured before and after sintering process. The trapped fields and temperatures were measured using a SQUID (Superconductor QUantum Interference Device) and  $J_c$  was estimated from the hysteresis loop using the extended bean model. The electrical resistivity was measured by using a standard four probe technique.

## 3. RESULTS AND DISCUSSION

Fig.1 (a) and (b) show the Full Width Half Maximum (FWHM) of XRD patterns at the main peak of mortar mixed samples and ball milled samples. The mortar mixing effect of  $\text{MgB}_2$  *ex-situ* powder at 1 h, 2 h and 10 h does not show much change in grains size compared to the pristine powder. On the other hand, it can be seen that from ball milling effect, remarkably the grain size decreases with the milling time increases. However the grains size remains the same after a milling time of 12 h. Fig.1 (c) shows X-ray diffraction patterns of samples after SPS using mortar mixed powder. As we can see, the  $\text{MgO}$ ,  $\text{MgB}_4$  and graphite peaks increase as the mixing time increases. We suggest  $\text{MgB}_2$  *ex-situ* powder reacts with air and/or water during the mixing process. Nevertheless, we expect that impurities that exist could act as pinning centres which could improve  $J_c$ .

Fig. 2 compares the temperature dependence on trapped fields,  $B_T$  for the  $\text{MgB}_2$  SPS pristine bulk, SPS mortar mixed bulk and SPS ball milled bulk with the CAP(capsule) and HIP(Hot Isostatic Pressure) method bulks between applies fields  $B_{ex}=5$  T. The SPS bulk using ball milled powder show the highest trapped

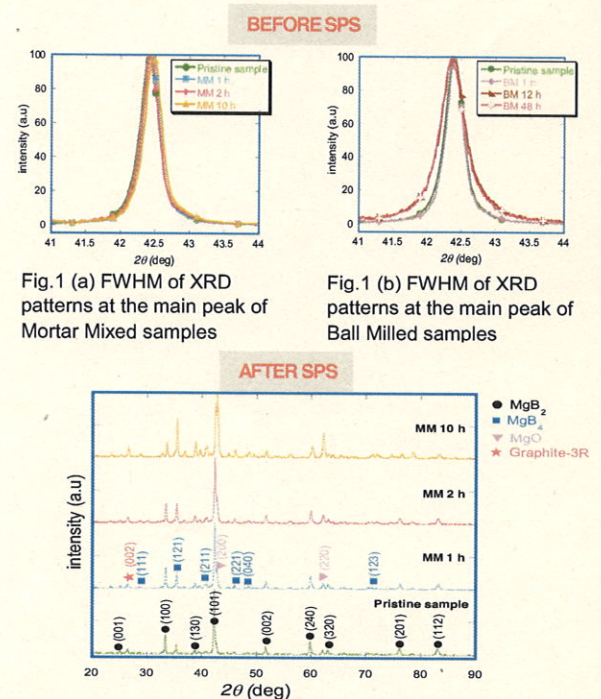


Fig.1 (c) XRD patterns of samples after SPS using pristine sample, and 1 h, 2 h, 10 h mortar mixed samples.



fields compared to SPS bulk using mortar mixed powder and shows about the same trapped field as a HIP bulk. For example, at 25 K, SPS ball milled bulk and HIP bulk show the same  $B_T=1.71$  T, instead SPS pristine bulk, SPS mortar mixed bulk and CAP bulk show  $B_T$  value 1.52 T, 1.39 T and 1.31 T respectively. We suggest that high trapped field of SPS bulk using ball milled powder was enhanced due to the enhancement of the grain growth and the grain boundaries effect of high energy impact of the ball milling.

Fig. 3 depicts the magnetic field dependence of the critical current density,  $J_c$  at 20 K for SPS bulk using pristine powder, SPS bulks using 1 h, 2 h and 10 h mortar mixed powders comparing with CAP and HIP bulks. At zero magnetic field ( $B=0$  T), HIP bulks shows the highest  $J_c$  value  $3.5 \times 10^5$  (A/cm<sup>2</sup>). CAP bulk and SPS bulks using 1h and 2 h mortar mixed powders show  $J_c$  values in the range  $1.4 \times 10^5 \sim 1.7 \times 10^5$  (A/cm<sup>2</sup>) and SPS bulk pristine powder shows a  $J_c$  value of  $4.7 \times 10^4$  (A/cm<sup>2</sup>). We realized that SPS bulks fabricated by mortar mixing powder and CAP method produced low  $J_c$  superconducting bulks compared to the HIP method. Furthermore, by increasing the mortar mixing time,  $J_c$  increases due to the coexistence of impurities constraining the magnetic flux lines in the bulk. However, for SPS bulk using 10 h mortar mixed powder shows the lowest  $J_c$ . We suggest even though many impurities exist, they do not act as the pinning centers for the bulk and just disturb the magnetic flux lines. In the future, we are planning to measure  $J_c$  for SPS bulks using ball milled powder. Related to the high  $B_T$  result of SPS bulk using ball milled powder, we expect it will show high  $J_c$  values too.

Fig. 4 presents the temperature dependences of the electrical resistivity for SPS bulk using pristine powder, SPS bulk using mortar mixed 1 h, 2 h and 10 h powders. The inset shows resistivity,  $\rho$  at 40 K and critical temperature,  $T_c$ . Besides, the electrical connectivity,  $\kappa$  which is the effective cross section of the bulk supercurrent path, was evaluated from the following equation,  $\kappa = (\Delta\rho_{\text{crystal}} / \Delta\rho_{\text{exp}}) \times 100\%$ , where  $\Delta\rho_{\text{crystal}} = 6.32 \mu\Omega\text{cm}$  and  $\Delta\rho_{\text{exp}} = \rho(300\text{K}) - \rho(40\text{K})$ , i.e., the ratio of the resistivity difference between the resistivity ideal of the ideal  $\text{MgB}_2$  grains and that of the present bulks. The connectivity value of SPS pristine, SPS mortar mixed 1 h, 2 h and 10 h are 5.4%, 32.7%, 18.7% and 6.5% respectively. Note that as the mortar mixing time increases, the  $\rho$  increases,  $T_c$  decreases and  $\kappa$  decreases due to the low purity of the  $\text{MgB}_2$  *ex-situ* powder after the mixing process. However, the SPS pristine sample shows the low  $T_c$ , highest  $\rho$  and the lowest  $\kappa$ . We expect that the bulk was not well-fabricated and some cracks may exist.

#### 4. CONCLUSION

In this study, to optimize the mixing and milling condition, we have investigated the trapped field and superconducting properties of  $\text{MgB}_2$  bulks fabricated by SPS method using several kinds of  $\text{MgB}_2$  *ex-situ* powder. Result of the X-ray diffraction, shows that the grain size decreases as the ball milling time increases. The optimal condition for ball-milling  $\text{MgB}_2$  *ex-situ* is 12h at 250 rpm. The mortar mixing results show as the mixing time increases,  $\text{MgO}$  and  $\text{MgB}_4$  peaks increase after SPS due to the reaction occurred during the mixing process. Using a SPS ball milling method, we are able to fabricate a bulk with high  $B_T$  which is similar to values attained in the bulk material fabricated by the HIP method, and this is due to an enhancement of the grain growth and the number of grain boundaries. Related to the high  $B_T$  result of SPS ball milled bulk, we expect it will show high  $J_c$  values too. Besides, mortar mixed bulks show as the mortar mixing time increases,  $J_c$  increases due to the coexistence of impurities acting as pinning centres in the bulk. Furthermore, the electrical resistivity result depicts the  $\rho$  increases,  $T_c$  decreases,  $\kappa$  decreases as the mortar mixing time increases due to low purity of the  $\text{MgB}_2$  *ex-situ* powder after mixing process.

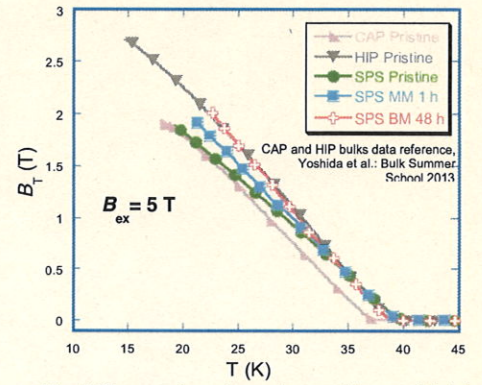
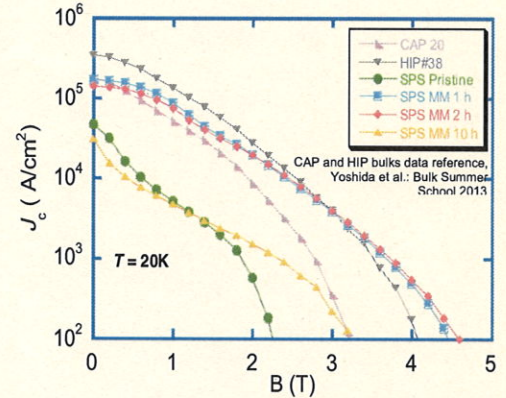


Fig. 2 Temperature dependence of trapped fields,  $B_T$  for  $\text{MgB}_2$  bulks with CAP, HIP and SPS fabrication methods at  $B_{\text{ex}} = 5$  T



current density,  $J_c$  at 20 K for SPS bulk using pristine powder, SPS bulks using 1 h, 2 h and 10 h mortar mixed powders comparing with CAP and HIP bulks

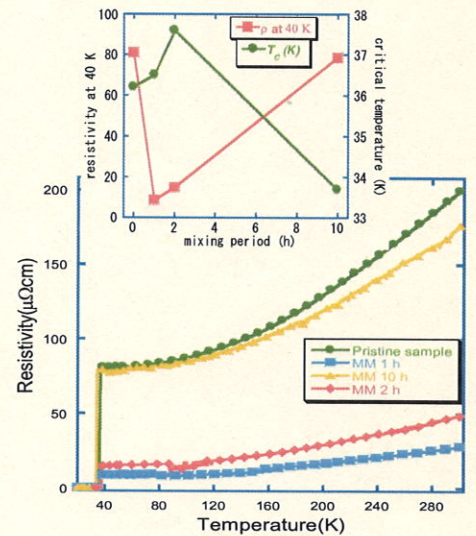


Fig. 4 Temperature dependences of the electrical resistivity for SPS pristine, SPS mortar mixed 1 h, 2 h and 10 h. The inset shows  $\rho$  at 40 K and  $T_c$  of the bulks.